



Modules for Maturing HVDC Electric Transmission Knowledge



Funded by the US Department of Energy (DOE) within the Office of Energy Efficiency & Renewable Energy (EERE)

# **HVDC-Learn Short Course**

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### Module 3d: Modular Multilevel Converter Design for HVDC Interface

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### Modular Multilevel Converter (MMC) Outline

### • Introduction

- Modular multilevel converter structure & operation principles
- Multilevel modulation methods
- Arm inductance impact & circulating current suppression
- Capacitor voltage balancing
- MMC-based HVDC system





## **Two Main HVDC Transmission Systems**

- HVDC Classic or Line Commutated Converters (LCC) HVDC Current source converters (CSCs) using controllable thyristor switches.
- Voltage source converters (VSC) HVDC

Pulse width modulated converters comprised of fully controllable switches like IGBTs or IGCTs. (In future, may be MMCs with SiC MOSFETs)



LCC HVDC Interface (Hitachi Energy)

VSC HVDC Interface (Hitachi Energy)





### **HVDC Converter Topologies**



### **HVDC Converters**



#### **Current Source Converter based HVDC**

- Line-commutated thyristor valves
- Power levels up to 6,400 MW
- Requires reactive power compensation
- Minimum short circuit capacity > 2X converter rating
- Power reversal with reversed DC link voltage polarity



Ref: [1] K. Johnson, "The ABCs of HVDC transmission technologies," *IEEE Power and Energy Magazine*, 2007. [2] J. G. Johansson, "HVDC converter technology." [Online]. Available: https://new.abb.com/docs/librariesprovider51/tillevenemang/jan-johansson\_hvdc-converter-technology.pdf?sfvrsn=2



### **HVDC Converters**

### Voltage Source Converter based HVDC



- Self-commutated IGBT valves
- Power levels up to 2000 MW
- Needs no reactive power compensation
- No minimum short circuit capacity
- Black start and improved AC fault ride-through capability
- Power reversal with reversed dc current polarity
- Fewer components; most equipment indoors



Ref: [1] K. Johnson, "The ABCs of HVDC transmission technologies," *IEEE Power and Energy Magazine*, 2007. [2] J. G. Johansson, "HVDC converter technology." [Online]. Available: https://new.abb.com/docs/librariesprovider51/tillevenemang/jan-johansson\_hvdc-converter-technology.pdf?sfvrsn=2



### **Comparison between Two Level VSC and MMC**



VSC based HVDC converter topologies



Ref: B. Gemmell, J. Dorn, D. Retzmann and D. Soerangr, "Prospects of multilevel VSC technologies for power transmission," 2008 *IEEE/PES Transmission and Distribution Conference and Exposition*, Chicago, IL, USA, 2008.



### **Multilevel Converter Applications**





Ref: Franquelo, L.G., J.Rodriguez, J.I. Leon, S. Kouro, R. Portillo, and M.A.M. Prats, "The Age of Multilevel Converters Arrives," *IEEE Industrial Electronics Magazine*, pp. 28-39, June 2008.



## **Multilevel Converter Topologies**

### General structure

- Synthesize desired ac voltage from several levels of dc voltages
- More levels produce a staircase waveform that approaches a sinusoid
- Harmonic distortion of output waveform decreases with more levels
- No voltage sharing problems with series connected devices
- $_{\circ}$  Low dv/dt reduces switching losses and EMI

### • Four structures

- Diode clamped converter
- Flying-capacitor converter
- Cascaded H-bridges inverter with separate dc sources
- Modular multilevel converter (MMC)









### **Cascaded H-Bridges Multilevel Inverter**





Single phase m-level structure



Ref. L. M. Tolbert, X. Shi, Y. Liu, "Multilevel Power Converters," *Power Electronics Handbook*, 5th Edition, 2023, ISBN 9780323992169, Chapter 12, pp. 407-435.



### Multilevel Converter Topologies – Clamping based



Three phase 6-level diode-clamped inverter with its multiplexer model

**Typical Applications:** 

- Static Var Compensation
- FACTs/UPC Applications
- Back-to-Back Intertie of Asynchronous AC Utilities



Three-phase 6-level flying capacitor inverter

- Interface between DC and AC •
- Interface between distributed • generation sources and utility
- Medium voltage motor drives •





Ref. L. M. Tolbert, X. Shi, Y. Liu, "Multilevel Power Converters," Power Electronics Handbook, 5th Edition, 2023, ISBN 9780323992169, Chapter 12, pp. 407-435.

## Multilevel Converter Topologies – Modular



Three phase wye connected **cascaded inverter** 



#### Modular multilevel converter (MMC)

### 

Ref. L. M. Tolbert, X. Shi, Y. Liu, "Multilevel Power Converters," *Power Electronics Handbook*, 5th Edition, 2023, ISBN 9780323992169, Chapter 12, pp. 407-435.

### **Typical Applications:**

- HVDC
- Static Var Compensator (SVC)
- STATCOM
- FACTS/UPFC Applications
- Active Power Filter
- Sag Compensation
- Interface with Distributed Generation Resources
  - Photovoltaics (Solar Panels)
  - Fuel Cells
  - Wind Turbines (rectified)
  - Energy Storage (Batteries, Ultracapacitors)



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### **MMC Structure**



## **MMC Configuration and Merits**



#### **Merits**:

- Modular design enables simple voltage scaling by a series connection of cells
- Filterless configuration
- High equivalent switching frequency for output voltage with relatively low individual device switching frequency



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### **MMC Sub-module Operation States**

State 1. Both IGBTs are switched off, often occurs during startup or fault condition.



State 2. IGBT  $T_1$  is switched ON, IGBT  $T_2$  is switched OFF, and the output voltage equals to the capacitor voltage  $u_c$ .



<u>State 3</u>. IGBT  $T_1$  is switched OFF, IGBT  $T_2$  is switched ON, and the output voltage is zero.



By adjusting the ON and OFF states of each switch, the desired sinusoidal voltage at the AC terminal can be achieved.





### **MMC** basic structure and operation principle

Power Electron. Appl., Barcelona, Spain, 2009, pp. 1-10.



The inner difference current of phase *j*,  $i_{diffi}$  is:



The output voltage is:

$$u_{vj} = \frac{u_{nj} - u_{pj}}{2} - \frac{R_0}{2} \cdot i_{vj} - \frac{L_0}{2} \cdot \frac{di_{vj}}{dt} \qquad (j = a, b, c)$$

$$R_0 \cdot i_{diffj} + L_0 \cdot \frac{di_{diffj}}{dt} = \frac{V_{dc}}{2} - \frac{u_{nj} + u_{pj}}{2} \quad (j = a, b, c)$$
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•  $L_0$  and  $R_0$  are the arm inductance and equivalent arm resistance.

- $V_{dc}$  and  $I_{dc}$  are the total dc bus voltage and dc current.
- $u_{vj}$  is the converter output voltage of *j* phase at point *v* and  $i_{vj}$  is the corresponding line current.
- The arm voltages generated by the cascaded SMs are expressed as  $u_{pj}$  and  $u_{nj}$  where the subscripts p and n denote the upper (positive) and lower (negative) arms, respectively.





### **Operation Principle**



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### **Multilevel Modulation Methods**





Ref: Franquelo, L.G., J.Rodriguez, J.I. Leon, S. Kouro, R. Portillo, and M.A.M. Prats, "The Age of Multilevel Converters Arrives," *IEEE Industrial Electronics Magazine*, pp. 28-39, June 2008.



## **Nearest Level Control (NLC)**

- The core idea of NLC is to first calculate how many sub-modules should be put into action.
- Capacitors' voltage sorting and final working sequence should be determined by the direction of the arm current.



#### Advantage:

Simple and using a low switching frequency.

#### Disadvantage:

There are frequent sorting issues with the capacitor voltage (sort from highest voltage to lowest voltage) which would be a burden to the controller if the number of sub-modules is large.





## **Carrier Level Shift PWM (CLS-PWM)**



- PD has the lowest line-to-line harmonic voltage distortion, while that of POD is the highest (APOD has the same harmonic components as CPS-PWM).
- Produces an uneven distribution of power among cells, which can produce a high harmonic content in the input current (especially when the modulation index is small).



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## **Carrier Phase Shift PWM (CPS-PWM)**



N+1 level modulation Shifted angle: 360°/N

2N+1level modulation Shifted angle: 180°/N

- Effective switching frequency of the load voltage is N times of the carrier wave, contributing to low switching losses
- Low harmonics contained in the output voltage enables smaller filter
- Offers an even power distribution among cells

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- Easy to be implemented independently between number of inverters
- Works in the over-modulation region when a common-mode term is added to the reference

Ref: B. P. McGrath and D. G. Holmes, "Multicarrier PWM strategies for multilevel inverters," *IEEE Transactions on Industrial Electronics,* vol. 49, no. 4, pp. 858–867, Aug. 2002.



### **CPS-PWM Modulation (2N+1 level)**



Modulation and carrier waves

Output phase voltage



Ref. L. M. Tolbert, X. Shi, Y. Liu, "Multilevel Power Converters," *Power Electronics Handbook*, 5th Edition, 2023, ISBN 9780323992169, Chapter 12, pp. 407-435.

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### **CPS-PWM Modulation (N+1 level)**

*N*=4 submodules,  $V_{dc}$ =240 V, arm inductance  $L_0$ =0 mH,  $f_c$ =1 kHz, amplitude modulation index =1, phase shift angle between carrier waveforms is 180°/4=45°, with resistive load and  $R_{load}$ =10  $\Omega$ .



Modulation and carrier waves





Ref. L. M. Tolbert, X. Shi, Y. Liu, "Multilevel Power Converters," *Power Electronics Handbook*, 5th Edition, 2023, ISBN 9780323992169, Chapter 12, pp. 407-435.

### **Modulation Methods Used in MMC**

#### Space-vector PWM (SVPWM)

#### Advantages:

- 1. Good utilization of dc-link voltage
- 2. Low switching frequency with reduced switching losses
- 3. Relatively easy hardware implementation by a digital signal processor (DSP)

#### Disadvantage:

1. As the number of levels increases, redundant switching states and the complexity of selecting switching states increase dramatically.



#### Selective Harmonic Elimination (SHE-PWM)

#### Advantage:

1. Up to N-1 harmonic contents can be removed from the voltage waveform.

#### Disadvantages:

- 1. If switching angles are computed offline and stored in tables, which are then interpolated according to the operating conditions, then can be used in open-loop or low-bandwidth applications.
- 2. Become very complex to design and implement for converters with a high number of levels (above five).



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Ref: José Rodríguez, Jih-Sheng Lai, and Fang Zheng Peng, "Multilevel Inverters: A Survey of Topologies, Controls, and Applications", *IEEE Trans. Ind. Electron.*, vol. 49, no. 4, pp. 724-738, August. 2002.

### **Comparison Between Modulation Methods**

Modulation methods	Advantages	Disadvantages	Application	
Nearest Level Control	Simplest; High voltage quality; Low switching losses	When modulation index and voltage levels are low, the THD increase significantly	High voltage level	
CPS-PWM	Low voltage distortion, easy to be modularized	Leads to circulating current between phases	Low and medium level	
CLS-PWM	Each carrier signal can be easily related to each power semiconductor	The vertical shifts produces an uneven power distribution among the cells	Low and medium level	
SVM	Simple, low voltage distortion;	High control complexity	Low voltage level	
SHE-PWM	Low voltage distortion	Poor dynamic response	Low voltage level	





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### **Circulating Current & Capacitor Voltages**

N+1 level modulation





Ref: Y. Li, "Arm Inductance and Sub-module Capacitance Selection in Modular Multilevel Converter," 2013.

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### Impact of Arm Inductors, $L_0$

*N*=4,  $V_{dc}$ =240 V, arm inductance  $L_0$ =2 mH,  $f_c$ =1 kHz, modulation index =1, phase shift angle between carrier waveforms is 360°/4=90°, with resistive load and  $R_{load}$ =10  $\Omega$ .





Spectrum analysis of the output voltage



Ref. X. Shi, Z. Wang, L. M. Tolbert, and F. Wang, "A comparison of phase disposition and phase shift PWM strategies for modular multilevel converters," in 2013 IEEE Energy Conversion Congress and Exposition, Sep. 2013, pp. 4089–4096.

### **Impact of Arm Inductors**



Larger arm inductance also helps to reduce the capacitor voltage unbalance and circulating current, but it increases system size, weight and cost.



Ref: Y. Li, "Arm Inductance and Sub-module Capacitance Selection in Modular Multilevel Converter," 2013.



### **Active Control Schemes**



#### Capacitor voltage control

Ref: Q. Tu, Z. Xu, and L. Xu, "Reduced Switching-Frequency Modulation and Circulating Current Suppression for Modular Multilevel Converters," IEEE Trans. Power Del., vol. 26, no. 3, pp. 2009 – 2017, July 2011.

![](_page_31_Figure_4.jpeg)

Ref: M. Hagiwara and H. Akagi, "Control and Experiment of Pulsewidth-Modulated Modular Multilevel Converters," IEEE Trans. Power Electron., vol. 24, no. 7, pp. 1737 –1746, July 2009.

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### **Circulating Current Control**

![](_page_32_Figure_1.jpeg)

✓ No additional hardware cost

![](_page_32_Picture_3.jpeg)

Ref. L. M. Tolbert, X. Shi, Y. Liu, "Multilevel Power Converters," *Power Electronics Handbook*, 5th Edition, 2023, ISBN 9780323992169, Chapter 12, pp. 407-435.

![](_page_32_Picture_5.jpeg)

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![](_page_33_Picture_7.jpeg)

![](_page_33_Picture_8.jpeg)

### **Capacitor Voltage Unbalance**

![](_page_34_Figure_1.jpeg)

![](_page_34_Picture_2.jpeg)

Ref: A. Ghazanfari and Y. A. R. I. Mohamed, "A Hierarchical Permutation Cyclic Coding Strategy for Sensorless Capacitor Voltage Balancing in Modular Multilevel Converters," IEEE J. Emerg. Sel. Top. Power Electron., vol. 4, no. 2, pp. 576–588, 2016.

![](_page_34_Picture_4.jpeg)

## **Capacitor Voltage Balancing**

60 58 Enabling balanced capacitor 56  $\Delta V_{ripple}$  $\Delta V_{2}$ voltages with small individual 54 Voltage (V) 52 level capacitors 50 48 46 44 ✓ No additional hardware cost 42 0.45 0.455 0.46 0.465 0.47 0.475 0.48 0.485 0.49 0.495 0.5 Time (s) 60 58 56 54 Voltage (V)  $\Delta V_1$ 52 Well-balanced case 50 48 46 44 42 0.45 0.455 0.46 0.465 0.470.475 0.48 0.485 0.49 0.495 0.5 Time (s)

![](_page_35_Picture_2.jpeg)

Not well-balanced case

Ref. L. M. Tolbert, X. Shi, Y. Liu, "Multilevel Power Converters," Power Electronics Handbook, 5th Edition, 2023, ISBN 9780323992169, Chapter 12, pp. 407-435,

![](_page_35_Picture_4.jpeg)

## **Classic Capacitor Voltage Balancing Methods**

![](_page_36_Figure_1.jpeg)

#### Classic closed-loop SM balancing method

Real-time SM voltage sampling Model-based estimation

Real-time arm current sampling Model-based arm current direction Offline net-charge change prediction

Reverse correspondence of SM voltages & switching pattern charging capability Non-global sorting and non-global pattern update Variable frequency switching Optimization of sorting process Model predictive control

![](_page_36_Picture_6.jpeg)

![](_page_36_Picture_7.jpeg)

Ref. S. Fan, L. M. Tolbert, X. Xiang, and W. Li, "Submodule Voltage Balancing Methods in Modular Multilevel Converters – A Review," in 2024 IEEE Energy Conversion Congress and Exposition (ECCE), Oct. 2024, pp. 2775–2782.

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![](_page_37_Picture_7.jpeg)

![](_page_37_Picture_8.jpeg)

### **MMC Based HVDC Transmission System**

![](_page_38_Figure_1.jpeg)

#### Differences from control of two level VSCs

- PWM signal generation
- Circulating current control •
- Capacitor voltage balancing control

![](_page_38_Picture_6.jpeg)

![](_page_38_Picture_7.jpeg)

### **Toshiba MMC-Based VSC for HVDC**

![](_page_39_Picture_1.jpeg)

Toshiba MMC-based Converter Valve

![](_page_39_Figure_3.jpeg)

Hokkaido-Honshu Japan HVDC Link (300MW, DC 250kV, DC 1200A)

Ref: https://www.global.toshiba/ww/products-solutions/transmission/products-technical-services/power-conversion.html/1000

![](_page_39_Picture_6.jpeg)

## Hitachi Energy (ABB) HVDC Light

![](_page_40_Picture_1.jpeg)

Power from Shore for Offshore Platforms

![](_page_40_Figure_3.jpeg)

![](_page_40_Picture_4.jpeg)

Hitachi Energy HVDC Light Valve Hall

Proposed Meshed Offshore HVDC Grid in Europe

![](_page_40_Picture_7.jpeg)

![](_page_40_Picture_8.jpeg)

### Siemens Energy HVDC Plus (MMC-based)

![](_page_41_Picture_1.jpeg)

2kA DC current 6.5kV voltage Half-bridge submodule

RENT

![](_page_41_Picture_3.jpeg)

![](_page_41_Picture_4.jpeg)

![](_page_41_Figure_5.jpeg)

BorWin3 (2019) project with float-over platform installation concept

![](_page_41_Picture_7.jpeg)

Ref: https://www.siemens-energy.com/us/en/home/products-services/product/hvdc-plus.html

### **Control System for HVDC PLUS**

![](_page_42_Figure_1.jpeg)

![](_page_42_Picture_2.jpeg)

Ref: B. Gemmell, J. Dorn, D. Retzmann and D. Soerangr, "Prospects of multilevel VSC technologies for power transmission," *IEEE PES Transmission and Distribution Conference and Exposition*, 2008, pp.1-16.

![](_page_42_Picture_4.jpeg)

## **Technology Evolution – Projects**

• First HVDC PLUS System (MMC): Trans Bay Cable Link, San Francisco

![](_page_43_Figure_2.jpeg)

- Rated power: 400 MW
- Reactive power: ± 300MVar
- DC voltage: ± 200 kV
- AC voltage: 230kV/138kV, 60Hz
- Transmission: 85 km submarine cable
- Commissioned: 2010

![](_page_43_Figure_9.jpeg)

![](_page_43_Picture_10.jpeg)

Ref : [1] H.-J. Knaak, "Modular multilevel converters and HVDC/FACTS: A success story," in *Proceedings of the 2011 14th European Conference on Power Electronics and Applications*, 2011. [2] A. Allerhand, "A Contrarian History of Early Electric Power Distribution [Scanning Our Past]," *Proceedings of the IEEE*, 2017.

![](_page_43_Picture_12.jpeg)

## **Technology Evolution – Projects**

• First VSC Project (MMC) with 1000 MW Capacity: INELFE (two links)

![](_page_44_Figure_2.jpeg)

- Rated power: 2\*1000 MW
- Reactive power: ± 300MVar
- DC voltage: ± 320 kV
- AC voltage: 400 kV, 50 Hz
- Transmission: 60 km underground cable
- Scheduled commission: 2014

![](_page_44_Picture_9.jpeg)

### **Space Savings in Comparison with HVDC "Classic"**

![](_page_45_Figure_1.jpeg)

![](_page_45_Picture_2.jpeg)

Ref: B. Gemmell, J. Dorn, D. Retzmann and D. Soerangr, "Prospects of multilevel VSC technologies for power transmission, "IEEE PES Transmission and Distribution Conference and Exposition, 2008, pp.1-16.

![](_page_45_Picture_4.jpeg)

### **Comparison of Three Generations of HVDC**

Application	Site footprint	Site area (%)	Max building height (%)	Converter building footprint	Converter building area (%)	Converter building volume (%)
LCC-HVDC	225 m	27,000 m <sup>2</sup>	20 m	35 m	700 m²	14,000 m²
(reference)	× 120 m	(100%)	(100%)	× 20 m	(100%)	(100%)
Two-level VSC	180 m	20,700 m²	24 m	38 m	1330 m²	25,000 m²
	× 115 m	(77%)	(120%)	× 35 m	(190%)	(179%)
Half-bridge	165 m	15,675 m²	15 m (75%)	70 m	2730 m <sup>2</sup>	29,500 m <sup>2</sup>
MMC-HVDC	× 95 m	(58%)		× 45 m	(390%)	(211%)

\* This comparison is made for comparable power and voltage ratings: for LCC-HVDC (Grita project, 500 MW and 400 kV), two-level VSC-HVDC (500 MW and 400 kV), and half-bridge MMC-HVDC (EWIC project, 500 MW and  $\pm$  200 kV)

![](_page_46_Picture_3.jpeg)

Ref: R. L. Sellick and M. Åkerberg, "Comparison of HVDC light (VSC) and HVDC classic (LCC) site aspects, for a 500MW 400kV HVDC transmission scheme," in *Proc. IET AC and DC Power Transmission*, 2012, pp. 1–6.

![](_page_46_Picture_5.jpeg)

### **Fault tolerant capacity**

![](_page_47_Figure_1.jpeg)

![](_page_47_Picture_2.jpeg)

Ref: B. Gemmell, J. Dorn, D. Retzmann and D. Soerangr, "Prospects of multilevel VSC technologies for power transmission, " IEEE PES Transmission and Distribution Conference and Exposition, 2008, pp.1-16.

![](_page_47_Picture_4.jpeg)

## Summary

- As power electronic switch ratings (IGBTs and SiC MOSFETs) increase, VSC-converter based HVDC interfaces are becoming more common.
- MMC-based converters have the advantages of modularity, redundancy, and low switching frequency.
- Need to consider switching (PWM) control method, capacitor voltage balancing, and circulating current suppression in design.
- Several companies offering MMC options for their VSC HVDC, SVC, and STATCOM products.

![](_page_48_Picture_5.jpeg)

![](_page_48_Picture_6.jpeg)

### **Acknowledgements**

![](_page_49_Picture_1.jpeg)

This work was supported primarily by the U.S. Department of Energy under DE-EE0011075.

![](_page_49_Picture_3.jpeg)

![](_page_49_Picture_4.jpeg)