

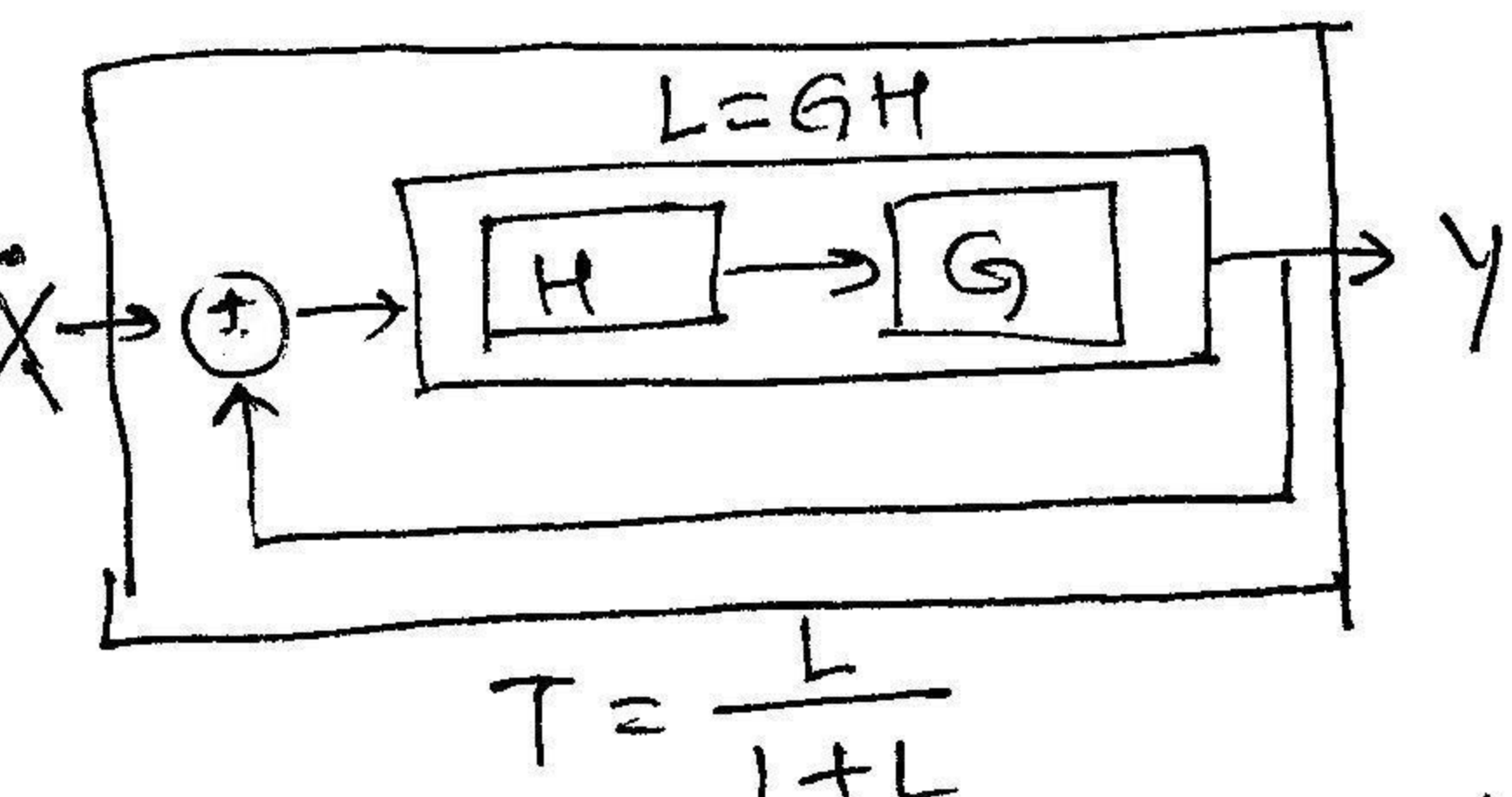
• Butterworth order-K low-pass filter: $|H(j\omega)|^2 = \frac{1}{1 + (\omega/\omega_c)^{2K}}$
with cut-off freq. = ω_c

• Given normalized low-pass filter, $\begin{cases} lp \rightarrow hp & s \rightarrow \frac{\omega_c}{s} \\ lp \rightarrow bp & s \rightarrow \frac{s^2 + \omega_0^2}{Bs} \\ lp \rightarrow br & s \rightarrow \frac{Bs}{s^2 + \omega_0^2} \end{cases}$

• FIR filter desired freq. response: $H_d(e^{j\Omega}) = H(e^{j\Omega}) e^{-j\Omega M/2}$ ($M = \text{window size}$)
 $h_{\text{FIR}}[n] = h_d[n] w[n]$

• IIR filter design: $H(j\omega) \xrightarrow{\text{analog filter design}} H(s) \xrightarrow{\text{filter design}} H(z)$
 $s = \frac{z-1}{T} \Rightarrow \omega = \frac{2}{T} \tan\left(\frac{\Omega}{2}\right)$ used for preserving critical freqs.

• T is sampling period and is found based on freq. of interest, say $[\omega_0, \omega_1]$
 $\Rightarrow T \leq \frac{2\pi}{2\omega_0} = \frac{\pi}{\omega_0}$ ($= \frac{2\pi}{\text{Bandwidth}}$)



sensitivity, $S = \frac{\Delta T/T}{\Delta G/G} = \frac{1}{1+L}$
Effect of noise, $Y = TX + \frac{1}{1+L} \text{ Noise}$

• Routh-Hurwitz: Analyze denominator of T to determine stability of T
• Root-locus: Plot of poles of T (as a function of loop-gain K of $L(s)$).
branches = max. num/den. degree; starts at poles of L , ends at zeros of L
asymptotes = #poles - #zeros; angles = $\frac{\text{odd multiples of } \pi}{\text{\# asymptotes}}$
meet at: $\frac{\text{sum}(\text{poles}) - \text{sum}(\text{zeros})}{\text{\# asymptotes}}$

breakaway point $\Rightarrow \left[\frac{d}{ds} \frac{1}{L(s)} = 0 \right]$ (converse need not hold)
angle criteria: $\text{Sum}(\text{pole angles}) - \text{Sum}(\text{zero angles}) = \text{odd multiple of } \pi$
magnitude criteria: $\text{product}(\text{pole distances}) / \text{product}(\text{zero distances}) = K$

Use Routh-Hurwitz to find poles on imaginary axis, and gain value there
• Nyquist plot: Plot of $L(j\omega)$ as ω ranges from $+\infty$ to $-\infty$ (K is fixed and given)
RHP poles of $T = \text{\# RHP poles of } L + \text{\# counterclockwise encirclement of } (-1, 0)$
• Gain margin = $\frac{1}{|L(j\omega_p)|}$ ($\angle L(j\omega_p) = \pi$) phase margin = $\angle L(j\omega_g) - \pi$ ($|L(j\omega_g)| = 1$)

Laplace Transforms

Signal	Transform	ROC
$x(t) = \frac{1}{2\pi j} \int_{\sigma-j\infty}^{\sigma+j\infty} X(s)e^{st} ds$	$X(s) = \int_{-\infty}^{\infty} x(t)e^{-st} dt$	
$u(t)$	$\frac{1}{s}$	$\text{Re}\{s\} > 0$
$tu(t)$	$\frac{1}{s^2}$	$\text{Re}\{s\} > 0$
$\delta(t - \tau), \tau \geq 0$	$e^{-s\tau}$	for all s
$e^{-at}u(t)$	$\frac{1}{s+a}$	$\text{Re}\{s\} > -a$
$te^{-at}u(t)$	$\frac{1}{(s+a)^2}$	$\text{Re}\{s\} > -a$
$[\cos(\omega_1 t)]u(t)$	$\frac{s}{s^2 + \omega_1^2}$	$\text{Re}\{s\} > 0$
$[\sin(\omega_1 t)]u(t)$	$\frac{\omega_1}{s^2 + \omega_1^2}$	$\text{Re}\{s\} > 0$
$[e^{-at} \cos(\omega_1 t)]u(t)$	$\frac{s+a}{(s+a)^2 + \omega_1^2}$	$\text{Re}\{s\} > -a$
$[e^{-at} \sin(\omega_1 t)]u(t)$	$\frac{\omega_1}{(s+a)^2 + \omega_1^2}$	$\text{Re}\{s\} > -a$

■ D.1.1 BILATERAL LAPLACE TRANSFORMS FOR SIGNALS THAT ARE NONZERO FOR $t < 0$

Signal	Bilateral Transform	ROC
$\delta(t - \tau), \tau < 0$	$e^{-s\tau}$	for all s
$-u(-t)$	$\frac{1}{s}$	$\text{Re}\{s\} < 0$
$-tu(-t)$	$\frac{1}{s^2}$	$\text{Re}\{s\} < 0$
$-e^{-at}u(-t)$	$\frac{1}{s+a}$	$\text{Re}\{s\} < -a$
$-te^{-at}u(-t)$	$\frac{1}{(s+a)^2}$	$\text{Re}\{s\} < -a$

Signal	Unilateral Transform $x(t) \xrightarrow{\mathcal{L}_u} X(s)$ $y(t) \xleftarrow{\mathcal{L}_u} Y(s)$	Bilateral Transform $x(t) \xleftarrow{\mathcal{L}} X(s)$ $y(t) \xrightarrow{\mathcal{L}} Y(s)$	ROC $s \in R_x$ $s \in R_y$
$ax(t) + by(t)$	$aX(s) + bY(s)$	$aX(s) + bY(s)$	At least $R_x \cap R_y$
$x(t - \tau)$	$e^{-s\tau}X(s)$ if $x(t - \tau)u(t) = x(t - \tau)u(t - \tau)$	$e^{-s\tau}X(s)$	R_x
$e^{s_0 t}x(t)$	$X(s - s_0)$	$X(s - s_0)$	$R_x + \text{Re}\{s_0\}$
$x(at)$	$\frac{1}{a}X\left(\frac{s}{a}\right), a > 0$	$\frac{1}{ a }X\left(\frac{s}{a}\right)$	$\frac{R_x}{ a }$
$x(t) * y(t)$	$X(s)Y(s)$ if $x(t) = y(t) = 0$ for $t < 0$	$X(s)Y(s)$	At least $R_x \cap R_y$
$-tx(t)$	$\frac{d}{ds}X(s)$	$\frac{d}{ds}X(s)$	R_x
$\frac{d}{dt}x(t)$	$sX(s) - x(0^-)$	$sX(s)$	At least R_x
$\int_{-\infty}^t x(\tau) d\tau$	$\frac{1}{s} \int_{-\infty}^0 x(\tau) d\tau + \frac{X(s)}{s}$	$\frac{X(s)}{s}$	At least $R_x \cap \{\text{Re}\{s\} > 0\}$

■ D.2.1 INITIAL-VALUE THEOREM

$$\lim_{s \rightarrow \infty} sX(s) = x(0^+)$$

This result does not apply to rational functions $X(s)$ in which the order of the numerator polynomial is equal to or greater than the order of the denominator polynomial. In that case, $X(s)$ would contain terms of the form $cs^k, k \geq 0$. Such terms correspond to the impulses and their derivatives located at time $t = 0$.

■ D.2.2 FINAL-VALUE THEOREM

$$\lim_{s \rightarrow 0} sX(s) = \lim_{t \rightarrow \infty} x(t)$$

This result requires that all the poles of $sX(s)$ be in the left half of the s -plane.

■ D.2.3 UNILATERAL DIFFERENTIATION PROPERTY, GENERAL FORM

$$\frac{d^n}{dt^n} x(t) \xrightarrow{\mathcal{L}_u} s^n X(s) - \frac{d^{n-1}}{dt^{n-1}} x(t) \Big|_{t=0^-} - s \frac{d^{n-2}}{dt^{n-2}} x(t) \Big|_{t=0^-} - \dots - s^{n-2} \frac{d}{dt} x(t) \Big|_{t=0^-} - s^{n-1} x(0^-)$$